

# Efficient Thermal Simulation in Metal Additive Manufacturing via Semi-Analytical Isogeometric Analysis

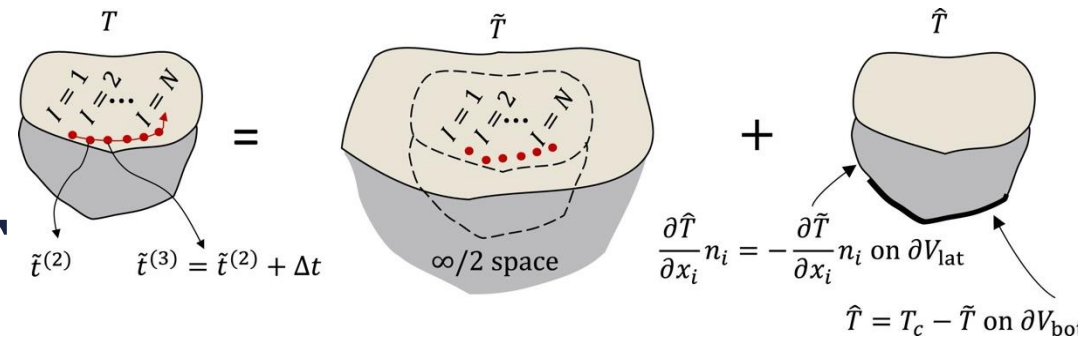
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# An analytical + correction split of T



**GOVERNING PROBLEM**

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T + Q / (\rho c_p) \quad \text{in } V$$

$$\frac{\partial T}{\partial n} = \theta \quad \text{on } \partial V_{\text{lat, top}}; \quad T = T_{\text{con}} \quad \text{on } \partial V_{\text{bot}}$$

**OUR DECOMPOSITION**

$$T = \tilde{T} + \hat{T}$$

- $\tilde{T}$  Analytical half-space field**  
Superposition of instantaneous point-source Green's functions. Closed-form, mesh-free, evaluated only where it matters.

$$\tilde{T}(\mathbf{x}, t) = \sum_{I=1}^K \frac{E^{(I)}}{\rho c_p [4\pi\alpha(t - \tau^{(I)})]^{3/2}} \exp\left(-\frac{\|\mathbf{x} - \mathbf{x}^{(I)}\|^2}{4\alpha(t - \tau^{(I)})}\right) H(t - \tau^{(I)})$$

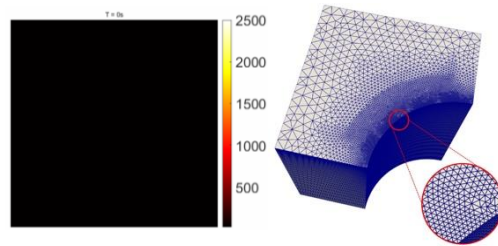
- $\hat{T}$  IGA correction field**  
A smooth NURBS solve of the heat equation whose boundary conditions cancel the half-space residual on the true geometry.

$$\rho c_p \frac{\partial \hat{T}}{\partial t} = k \nabla^2 \hat{T}, \quad \frac{\partial \hat{T}}{\partial n} = -\frac{\partial \tilde{T}}{\partial n} \quad \text{on } \partial V_{\text{lat}} \cup \partial V_{\text{top}}, \quad \hat{T} = T_c - \tilde{T} \quad \text{on } \partial V_{\text{bot}}.$$

*Heat-source agnostic — any kernel admitting a half-space solution (Gaussian surface source shown).*

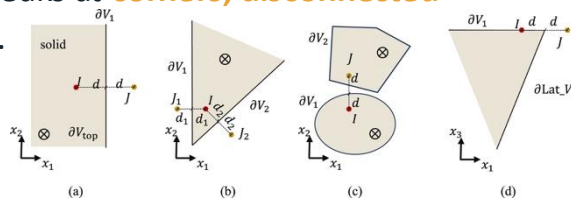
## THE BOTTLENECK

LPBF drives steep gradients on the scale of the laser spot,  $r \approx 20 \mu\text{m}$ . FEM then needs uniformly fine meshes or scan-wise remeshing — **intractable at part scale.**



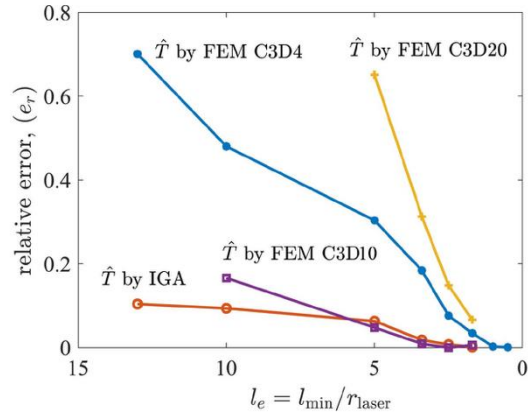
## WHY IMAGE-SOURCES FAIL

The classical image-source method enforces adiabatic walls only for prismatic blocks. On real CAD it breaks at **corners, disconnected solids, and varying cross-sections.**

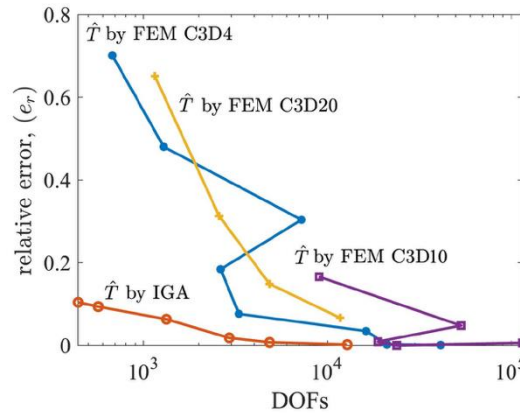


# Matched accuracy at a fraction of the cost

Relative  $L^2$ -error of the total field  $T$

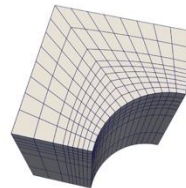
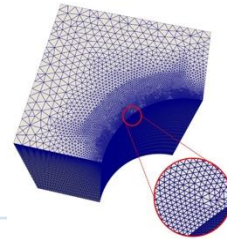


vs element size  $l_e = l_{min}/r$



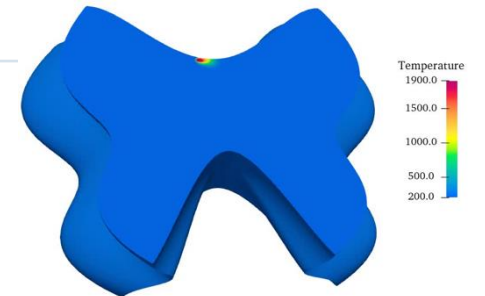
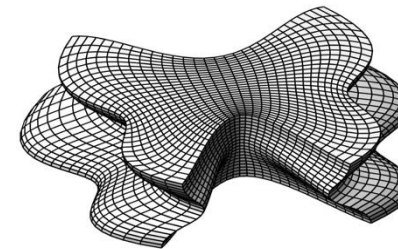
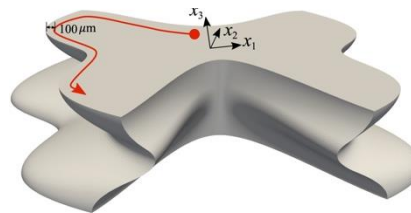
vs degrees of freedom

IGA holds  $e_r \lesssim 10\%$  even at  $l_e = 13$  (elements 13× the laser radius), and sits **1–2 orders of magnitude** below FEM at matched DOFs.



$C^{p-1}$  NURBS resolve through-thickness gradients smoothly across coarse elements — where  $C^0$  FEM must keep refining  $l_{min}$ .

**Generalises to free-form CAD:** adiabatic BCs enforced on a butterfly part (cubic-NURBS, 27 456 DOFs) where image-sources are inapplicable.



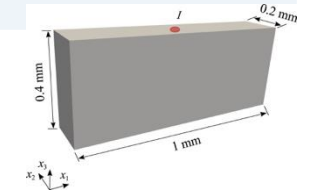
**80×**

vs Abaqus C3D4

**258×**

vs Abaqus C3D20

CPU / step at matched 5% error



Thin-wall benchmark (uniform mesh,  $e_r \leq 5\%$ )

Method	DOFs	CPU/step
IGA (G+Smo, quad.)	2 639	<b>0.132 s</b>
Abaqus C3D4	11 536	10.6 s
Abaqus C3D20	45 261	34.0 s